# Proposed Redevelopment Preliminary Geotechnical Investigation Report

182-186 Gertrude St North Gosford

80021082

Prepared for Lindfield Group Pty Ltd

24 July 2022





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Gosford

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## **Document History**

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## 1 Introduction

As requested, a senior geotechnical engineer from Cardno attended site on the 13<sup>th</sup> July 2022. The purpose of this investigation was to assess the site's surface and subsurface conditions in order to provide recommendations from a geotechnical viewpoint for the design and construction of the proposed new residential apartment development. The results of the investigation are detailed below.

#### 1.1 Available Information

At the time of preparing this report, the following info are made available for review:

 Architecture plans, prepared by Texco Design, dated 7/04/2022, rev D, showing the proposed building and basement footprints.

#### 1.2 Proposed Development

At the time of preparing this report, we understand that the proposed residential redevelopment includes:

- The demolition of the existing three (3) dwellings at 182, 184, and 186 Gertrude St, North Gosford.
- Construction of proposed seven storey apartments with basements. Based on the information provided, it is anticipated that the proposed basement excavation will be up to 13m deep.

## 2 Findings of Investigation

#### 2.1 Geological Condition

Reference to the Geological Map of Gosford to Lake Macquarie (1:100,000) indicates that the site is underlain of Terrigal Formation (Rnt) which comprises interbedded laminite, shale and quartz, to lithic-quartz sandstone.

Geological plan of the site is shown in Appendix A.

#### 2.2 Fieldwork

Fieldwork for the geotechnical investigation was carried out on 13th July 2022 and comprised the following:

- A detailed walkover inspection of the site and surrounds.
- Drilling of a total of four (6) boreholes (HA1 to HA6 inclusive) across the site, using manual hand auger equipment taken to target depths of about 1m.
- In-situ testing using a Dynamic Cone Penetrometer (DCP) was conducted across the site. Six (6) DCP tests were undertaken up to 2.5m depth to weathered sandstone / siltstone bedrock refusal.

The approximate borehole and DCP test locations are shown on the enclosed Borehole and DCP test location plan referenced as Figure 1 in Appendix A.

#### 2.3 Site Description

The following site observation were made:

- The site is rectangular in shape, and is currently occupied by three (3) dwellings. The buildings are currently occupied and appears to be in a moderate condition.
- The site is bounded by Gertrude St to the east and residential properties on the other sides. No basements were observed on the adjoining properties Nos 178 and 188-198 Gertrude St.
- Site slopes down from east to west, with surveyed RL at the east approximately 40.42 m slopping towards the west to approximate RL of 32.27 m, at a degree of about 10 degrees.



#### 2.4 Surface Condition

Based on the observations from the geotechnical investigation, the sub surface profile within the footprint of the proposed development can be generalised as follows:

- Topsoil Sandy Clay and Clayey Sand, fine to medium grained, low to medium plasticity clay, dark brown, 0.1m thick, grass covered, overlying,
- Fill Sandy Clay and Clayey Sand, fine to medium grained Sand, low to medium plasticity, dark brown with gravel, 0.2-0.5m thick across the site, overlying,
- Silty Clay, medium to high plasticity, brown, with sand and gravel, overlying weathered siltstone / sandstone bedrock.

Based on findings of investigation, weathered siltstone bedrock is expected at depths of 0.5-1.5m at the eastern half of site, and 1.5-2.5m at the western half of the site.

The encountered subsurface materials and their relative strengths have been recorded and logged as Engineering Log of Boreholes in accordance with AS 1726:2017 Geotechnical Site Investigation and on a Penetration Resistance of Soil Test Sheet. These have been enclosed in Appendix B.

A typical Gosford station area borehole based on past experience is shown below:



#### 2.5 Groundwater Condition

Groundwater table or seepage was not encountered in any of the boreholes during drilling to shallow depths of not more than about 1m below existing ground surface levels. Based on the findings, surrounding landform, and past nearby project experience, it is anticipated the proposed 13m basement earthwork is unlikely to intersect with the groundwater table at the subject site. However, it is possible that localised seepage may occur within interface of soils and rocks and fractures and defects of rock when an intense and prolonged rainfall occurs during excavation.



## 3 Comments and Recommendations

#### 3.1 General

It is understood that the proposed development comprises of demolishing the existing dwellings across three (3) sites and constructing new seven storey apartment with basements. Excavation will include cutting into the existing slope of up to 13m, and general site levelling.

#### 3.2 Excavation Condition

We expect overburden soils comprising topsoil, sand fill, and weathered siltstone / sandstone in the upper 2m section to be readily excavated by conventional earthworks equipment such as excavators. Ripping or hammering will be required for any deeper bulk excavation into the less weathered siltstone / sandstone materials. Therefore, the induced vibration level control will be required to avoid impacting the adjacent properties.

Induced vibrations in structures adjacent to the excavation should not exceed a Peak Particle Velocity (PPV) of 10mm/sec for brick or unreinforced structures in good condition.

To ensure vibration levels remain within acceptable levels and minimise the potential effects of vibration, excavation into medium or higher strength siltstone / sandstone across the site should be complemented with saw cutting or other appropriate methods prior to excavation. Rock saw cutting should be carried out using an excavator mounted rock saw, or the like, so as to minimise transmission of vibrations to any adjoining properties.

If vibrations in adjacent structures exceed the values recommended above or appear excessive during construction, excavation should cease and the project Geotechnical Engineer should be contacted immediately for appropriate reviews so that counter measures/actions can be taken.

We recommend that dilapidation surveys of the adjacent structures be carried out prior to earthwork commencement.

We recommend that inspections be carried out by a Geotechnical Consultant at every 1.5m deep intervals during excavation to assess excavation stability.

#### 3.3 Site Classification

Based on the results of this investigation, we consider that the subsurface conditions comprise topsoil overlying most sand and rock. A site classification of "Class A – Most sand and rock sites with little or no ground movement from moisture changes" can be adopted (if applicable) for footings constructed in accordance with AS2870-2011.

#### 3.4 Groundwater Conditions

It is anticipated the proposed earthwork will not intersect with the groundwater table. However, localised seepage may occur within interface of soils and rocks and fractures and defects of rock when an intense and prolonged rainfall occurs during basement excavation. It is anticipated the potential to occur large amount of inflow through soils, interface of soils and rocks, and through joints within shale is minor during basement excavation. The conventional pump and sump method is considered manageable of such inflow water.

We also recommend the following control measures during design and construction:

- Strip drains, weepholes, subsoil drains, drainage materials should be included in the design of shoring and retaining walls.
- Collection trenches or pipes and pits connected to the building stormwater system. A stormwater storage tank and pump system may be required.
- The basement walls and slabs should be designed to withstand hydrostatic pressures taking into consideration the potential for seepage.
- Seepage or subsurface runoff inside the excavated foundation pits or pile holes should be removed prior to pouring of concrete.



## 3.5 Temporary Batter Slopes

Considering the proposed offset distance and depths of bedrock, piled retaining structure is recommended prior to basement excavation, temporary batter slopes may not be appropriated.

#### 3.6 Retaining Structures

Shoring and support basement excavation and control lateral ground movement are recommended. The options include the following:

- Soldier pile wall shoring system; or
- Contiguous or semi-contiguous cast in-situ reinforced concrete piles embedded into underlying Class III Sandstone or better rock, and gaps between the piles should be covered with reinforced shotcrete or reinforced concrete panels.

Temporary anchorage or other temporary tie-back system may be required to be installed prior to excavation to reduce the potential effects of ground movement on adjoining properties. Typically, anchors are to be installed at regular intervals along the shoring wall. However, installation of anchors beyond the property boundaries will be subject to approval by owners of adjoining properties or public assets. If installation of temporary anchors is not feasible, it is necessary to consider other options to control lateral ground movement. These options include the following:

- Temporary solutions such as installation of props associated with staged excavation; or
- Staged excavations and creating temporary partial berms in front of walls.

It is recommended that monitoring of ground movement (settlement and deflection) should be carried out during excavation.

During basement excavation, observations and recording on conditions of exposed faces should be carried out by the project Geotechnical Engineer, so that loose materials or weak

The retaining wall should be designed and constructed in accordance with AS4678 Earth- Retaining Structures.

The recommended preliminary parameters for design of retaining structures are presented in Tables 3-1 and 3-2 below. The coefficients provided are based on drained conditions. Rock classification and depths are to be determined in future study.

Table 3-1 Preliminary Geotechnical Design Parameters for Retaining Walls

Geotechnical Unit	Unit Weight (kN/m³)	Effective Cohesion c' (kPa)	Angle of Effective Internal Friction <i>∜</i> (degre)	Modulu s of Elasticit y E <sub>s (h)</sub> (MPa)	Poisson Ratio v
Fill (Unit 1)	17	2	27	8	0.35
Residual Soils (Unit 2)	18	18 5		20	0.35
Class V Siltstone / Sandstone (Unit 3a)	22	50	28	100	0.35
Class IV/III Siltstone / Sandstone (Unit 3b)	24	200	32	500	0.20

Table 3-2 Preliminary Coefficients of Lateral Earth Pressure

Geotechnical Unit	Coefficient of Active Lateral Earth Pressure (Ka)	Coefficient of Lateral Earth Pressure at Rest (Ko)	Coefficient of Passive LateralEarth Pressure (K)
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Fill (Unit 1)	0.38	0.55	2.7
Residual Soils (Unit 2)	0.36	0.53	2.8
Class V Siltstone / Sandstone (Unit 3a)	0.36	0.53	2.8
Class IV/III Siltstone / Sandstone (Unit 3b)	0.31	0.47	3.3

The foregoing coefficients assume that the ground level behind the retaining structures is horizontal and the retained material is effectively drained. Adequate surface and sub-surface drainage is to be provided behind retaining walls.

Surcharge loading from neighbouring structures should also be taken into account in the design of retaining structures should it be within the zone of influence of the excavation. The zone of influence of the excavation is defined as a plane projected at 45 degrees from horizontal from the toe of the excavation face upwards into the excavation face towards the ground surface.

For design of temporary ground anchors, the allowable bond stress of 20kPa, 50kPa, and 200kPa, can be adopted within Residual Soils (Unit 2), Class V Siltstone / Sandstone (Unit 3a), and Class IV/III Siltstone / Sandstone (Unit 3b) respectively. The following is recommended as a guidance for anchor design:

- Anchor bond length of at least 3m behind the "active" zone of the excavation;
- Overall stability of anchor system and interaction is satisfactory; and
- The anchors are proof loaded to at least 1.3 times the design working load before locking off at working load.
- Deflection to be monitored within the TfNSW limit.

## 3.7 Structural Footings

It is anticipated that the proposed bulk earthwork basement is likely to be founded predominantly in Class IV / III Siltstone / Sandstone (Units 3b) bedrock.

It is assessed that a foundation system consisting of cast-in-situ reinforced concrete shallow foundations, such as pad or strip footings under columns and walls, would be applicable for the proposed development at this site.

Installation of piles is expected to be required for excavation shoring walls and in case of large axial loads on columns and walls and exceeding the bearing pressure of the bearing stratum. Other cases where piles may be required include the need to increase the stiffness of the founding rock, or increase the resistance against lateral seismic loads. Piles are expected to be socketed into underlying rock better than Class III/IV Siltstone Sandstone (Unit 3b). Bored piles would be applicable for this site.

The geotechnical capacities and parameters recommended for design of shallow and piled foundations are provided in Table 3-3 below:

Table 3-3 Preliminary Geotechnical Foundation Design Capacities and Parameters

Geotechnical Unit	Allowable End BearingPressure kPa <sup>1</sup>	Allowable Shaft Adhesion Compression <sup>2</sup> kPa	Modulus of Elasticity Es,v (MPa)		
Fill (Unit 1)	N/A³	N/A³	N/A³		
Residual Soils (Unit 2)	N/A³	20	25 150		
Class V Siltstone / Sandstone (Unit 3a) <sup>4</sup>	600 (shallow footing)	40			
Class IV/III Siltstone / Sandstone (Unit 3b) <sup>4</sup>	2500 (shallow footing) 3000 (piles)	150	600		



#### Notes:

- 1 With a minimum embedment depth of 0.8m for piled foundations and 0.5m for shallow foundations.
- 2 Shaft Adhesion applicable to piles only.
- 3 N/A, Not Applicable or being excavated or not recommended for the proposed development.
- 4 The actual depth of underlying Class V Sandstone to Class III Sandstone should be confirmed during construction.

To minimise the potential effects of differential settlement under the buildings loads, it is recommended all foundations of the proposed building should be founded on consistent materials of similar properties or rock of similar class.

Shaft adhesion may be applied to socketed piles adopted for foundations if socket shaft lengths conform to appropriate classes of sandstone and accepted levels of shaft sidewall cleanliness and roughness. The rock socket sidewalls should be free of soil and/or crushed rock to the extent that natural rock is exposed over at least 80% of the socket sidewall. Shaft adhesion should be reduced or ignored within socket lengths that are smeared and fail to satisfy cleanliness requirements. Additional attention to cleanliness of socket sidewalls may be required where presence of clay seams and weathered sandstone bands is evident over socket lengths.

Any water, debris, loose and wet materials should be wholly removed from excavated footing areas prior to pouring of concrete.

We recommend that footing inspections be carried out by a Geotechnical Engineer / consultant during footing excavation to confirm appropriate founding materials, that the recommended serviceability bearing pressures could be met and to ensure that all soft and wet materials have been removed from the foundation footprint prior to concrete placement.

#### 3.8 Future Assessment

It is considered that the subject site is suitable for the proposed residential development. In order to inform for the detailed design assessment, it is recommended that supplementary geotechnical assessment to be carried out, including:

- Additional cored borehole across the site, to at least 5m below the proposed design bulk excavation level for rock classification;
- Installation of groundwater monitoring wells. Testing of groundwater seepage water aggressivity and rates
- Prior to construction commencement, numerical modelling of the eastern shoring wall adjacent to Gertrude St (TfNSW asset) and southern shoring wall adjacent to the adjoining property, to assess the likely amount of excavation-induced ground movement as a result of the proposed excavation. Preparation of monitoring plan; and
- Waste classification of all material to be excavated and transported off site.

## 4 Limitation

Assessment of the sub-surface profile at the site and the recommendations presented in this report are based on information from six (6) boreholes, drilled at locations considered representative across the site, and DCP testing at six (6) locations. Based on the results of the investigation and subsurface variability, there is a possibility that actual geotechnical conditions across the site could differ from the inferred geotechnical model presented in this report.

This report contains geotechnical parameters to be used as input for the structural design of footings and retaining walls. On-going geotechnical input is required to ensure recommendations provided in this report are followed and that actual ground conditions reflect those indicated in this report. In the absence of adequate information about the siting, extent and depth of the proposed earthwork, it is mandatory that a review of the recommendations as presented in this report, are carried out upon finalisation of the earthwork design, prior to any excavations.

APPENDIX



SITE PLAN







APPENDIX

B

BOREHOLE LOGS





## PENETRATION RESISTANCE OF SOIL TEST FIELD SHEET



Project:				-	Project No.			Testing Type									
Proposed Redevelopment					80021088			Dynamic Cone Penetrometer (DCP)						х			
Client:						-	Test By:		-	Dynamic Perth Sand Penetrometer (PSP)							
							AT										
Location:				•	Date:		Location:			Sheet:							
182,184,186 Gertrude St, North Gosford				13/07/2022			Refer to S	Site Plan				1	I				
	1		1	1	1		1	1	1	1	1		1		1	ı	1
DCP No.	DCP1	DCP2	DCP3	DCP4	DCP5		DCP6										
Penetration (mm)	Numbe	r of Blows	s per 150	mm Pene	etration	Penetration (mm)				ws per 150 mm Penetration Penetration (mm)			Number of Blows per 150 n			mm Penetration	
150	1	0	3	1	1	150	1					150					
300	2	1	4	1	2	300	1					300					
450	4	3	5	3	3	450	3					450					
600	6	3	6	3	3	600	3					600					
750	10	7	12	6	8	750	6					750					
900	13	7	25	8	8	900	8					900					
1050	16	12	R	12	12	1050	10					1050					
1200	25	17		19	19	1200	17					1200					
1350	R	19		33	25	1350	25					1350					
1500		16		R	R	1500	R					1500					
1650		19				1650						1650					
1800		22				1800						1800					
1950		18				1950						1950					
2100		20				2100						2100					
2250		26				2250						2250					
2400		34				2400						2400					
2550		R				2550						2550					
2700						2700						2700					
2850						2850						2850					
3000						3000						3000					
3150						3150						3150					
3300						3300						3300					
3450						3450						3450					
3600						3600						3600					
							Test Pro	ocedure: A	AS 1289.6.	3.2							

#### PIT NO : HA1 **EXCAVATION - GEOLOGICAL LOG** FILE / JOB NO : PROJECT: 182,184,186 Gertrude St, North Gosford LOCATION: North Gosford SHEET: 1 OF 1 POSITION: E: 346203.310, N: 6301115.880 (56 MGA94) SURFACE ELEVATION: 39.400 (AHD) EQUIPMENT TYPE: Hand Auger METHOD: Hand Auger DATE EXCAVATED: 13/7/22 LOGGED BY: AT CHECKED BY: TH **EXCAVATION DIMENSIONS DRILLING** MATERIAL 100 200 HAND 300 & PENETRO-300 W METER CONSISTENCY RELATIVE DENSITY DCP TEST AS 1289.6.3.2-1997) Blows/150 mm MOISTURE SAMPLES & FIELD TEST Ξ SUPPORT GRAPHIC MATERIAL DESCRIPTION PENETRAT 500 DEPTH ( STRUCTURE Soil Type, Colour, Plasticity or Particle Characteristic Secondary and Minor Components & Other Observations 0.0 SANDY CLAY: dark brown, low to medium plasticity, fine to medium grained sand, with fine to medium grained gravel, with rootlets TOPSOIL STABLE FILL FILL: SANDY CLAY: dark brown, low to medium plasticity, fine to medium grained sand, with fine to М medium grained gravel RESIDUAL SOIL SILTY CLAY: brown, pale brown, medium to high plasticity, with fine to medium grained sand St 0.5 Sandy SILT: pale brown-orange, fine to medium grained sand, with low plasticity silt, inferred as very low strength highly weathered siltstone WEATHERED ROCK EXCAVATION HA1 TERMINATED AT 1.00 m 1.5 2.0 2.5 3.0 PHOTOGRAPHS NOTES YES NO NO CLASSIFICATION SYMBOLS & SOIL DESCRIPTION CONSISTENCY/ METHOD PENETRATION SAMPLES & FIELD TESTS RELATIVE DENSITY ᄪᄪᄑᅗ VS S F St Based on Unified - Very Soft - Soft U50 - Undisturbed Sample Natural Exposure No Resistance Classification System 50 mm diameter Existing Excavation - Firm - Stiff Disturbed Sample BH Backhoe Bucket MOISTURE - Very Stiff - Hard В **Bulk Disturbed Sample** VSt Bulldozer Blade H VL MC Moisture Content D - Dry M - Moist W - Wet Ripper WATER - Very Loose - Loose Hand Penetrometer (UCS kPa) 10 Oct., 73 Water Level on Date shown VS Vane Shear; P-Peak MD D VD

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Plate Bearing Test

PBT

R-Remouded (uncorrected kPa)

EXCAVATION NORTH GOSFORD.

RMS LIB 40.3

SUPPORT

Timbering

See Explanatory Notes for details of abbreviations

& basis of descriptions.

water inflow

water outflow

- Medium Dense

- Dense - Very Dense

#### PIT NO: HA2 **EXCAVATION - GEOLOGICAL LOG** FILE / JOB NO : PROJECT: 182,184,186 Gertrude St, North Gosford LOCATION: North Gosford SHEET: 1 OF 1 POSITION: E: 346168.830, N: 6301121.370 (56 MGA94) SURFACE ELEVATION: 33.800 (AHD) EQUIPMENT TYPE: Hand Auger METHOD: Hand Auger DATE EXCAVATED: 13/7/22 LOGGED BY: AT CHECKED BY: TH **EXCAVATION DIMENSIONS DRILLING** MATERIAL 100 200 HAND 300 & PENETRO-300 W METER CONSISTENCY RELATIVE DENSITY MOISTURE DCP TEST AS 1289.6.3.2-1997) Blows/150 mm PENETRATION SAMPLES & FIELD TEST DEPTH (m) SUPPORT GRAPHIC MATERIAL DESCRIPTION 500 STRUCTURE Soil Type, Colour, Plasticity or Particle Characteristic Secondary and Minor Components & Other Observations 0.0 SANDY CLAY: dark brown, low to medium plasticity, fine to medium grained sand, with fine to medium grained gravel, with rootlets TOPSOIL STABLE FILL FILL: SANDY CLAY: dark brown, low to medium plasticity, fine to medium grained sand, with fine to medium grained gravel М 0.5 ğ SILTY CLAY: brown, pale brown, medium to high plasticity, with fine to medium grained sand RESIDUAL SOIL VSt EXCAVATION HA2 TERMINATED AT 1.00 m 1.5 2.0 2.5 3.0 PHOTOGRAPHS NOTES YES NO NO CLASSIFICATION SYMBOLS & SOIL DESCRIPTION CONSISTENCY/ METHOD PENETRATION SAMPLES & FIELD TESTS RELATIVE DENSITY <u>шшт</u>= VS S F St Based on Unified - Very Soft - Soft U50 - Undisturbed Sample Natural Exposure No Resistance Classification System 50 mm diameter Existing Excavation - Firm - Stiff Disturbed Sample BH Backhoe Bucket MOISTURE VSt H VL - Very Stiff - Hard В **Bulk Disturbed Sample** Bulldozer Blade MC Moisture Content D - Dry M - Moist W - Wet Ripper WATER - Very Loose - Loose Hand Penetrometer (UCS kPa) 10 Oct., 73 Water Level on Date shown VS Vane Shear; P-Peak MD D VD SUPPORT - Medium Dense R-Remouded (uncorrected kPa) water inflow - Dense - Very Dense Timbering PBT - Plate Bearing Test water outflow See Explanatory Notes for

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EXCAVATION NORTH GOSFORD.GPJ

RMS LIB 40.3

details of abbreviations

& basis of descriptions.

#### PIT NO : HA3 **EXCAVATION - GEOLOGICAL LOG** FILE / JOB NO : PROJECT: 182,184,186 Gertrude St, North Gosford LOCATION: North Gosford SHEET: 1 OF 1 POSITION : E: 346202.060, N: 6301091.120 (56 MGA94) SURFACE ELEVATION: 38.300 (AHD) EQUIPMENT TYPE: Hand Auger METHOD: Hand Auger DATE EXCAVATED: 13/7/22 LOGGED BY: AT CHECKED BY: TH **EXCAVATION DIMENSIONS DRILLING** MATERIAL 100 200 HAND 300 & PENETRO-300 W METER CONSISTENCY RELATIVE DENSITY MOISTURE DCP TEST AS 1289.6.3.2-1997) Blows/150 mm PENETRATION SAMPLES & FIELD TEST DEPTH (m) SUPPORT GRAPHIC MATERIAL DESCRIPTION 500 STRUCTURE Soil Type, Colour, Plasticity or Particle Characteristic Secondary and Minor Components & Other Observations 0.0 SILTY CLAYEY SAND: dark brown, fine to medium grained sand, low to medium plasticity clay, with fine to medium grained gravel, with rootlets TOPSOIL STABLE FILL FILL: SILTY CLAYEY SAND: dark brown, fine to medium grained sand, fine to medium grained clay М RESIDUAL SOIL SILTY CLAY: brown, medium to high plasticity, with fine to medium grained sand М St 0.5 ğ SILTY CLAY: pale brown, yellow, mottled red, medium to high plasticity /St to H EXCAVATION HA3 TERMINATED AT 1.00 m 1.5 2.0 2.5 3.0 PHOTOGRAPHS NOTES YES NO NO CLASSIFICATION SYMBOLS & SOIL DESCRIPTION CONSISTENCY/ METHOD PENETRATION SAMPLES & FIELD TESTS RELATIVE DENSITY VS S F St Based on Unified - Very Soft - Soft U50 - Undisturbed Sample Natural Exposure No Resistance Classification System 50 mm diameter Existing Excavation - Firm - Stiff Disturbed Sample BH Backhoe Bucket MOISTURE VSt H VL - Very Stiff - Hard В **Bulk Disturbed Sample** Bulldozer Blade MC Moisture Content D - Dry M - Moist W - Wet Ripper WATER - Very Loose - Loose

CARDNO NSW/ACT PTY LTD

Vane Shear; P-Peak

- Plate Bearing Test

VS

PBT

10 Oct., 73 Water Level on Date shown

water inflow

water outflow

Hand Penetrometer (UCS kPa)

R-Remouded (uncorrected kPa)

EXCAVATION NORTH GOSFORD.GPJ

RMS LIB 40.3

SUPPORT

Timbering

See Explanatory Notes for details of abbreviations & basis of descriptions.

MD D VD

- Medium Dense - Dense - Very Dense

#### PIT NO : HA4 **EXCAVATION - GEOLOGICAL LOG** FILE / JOB NO : PROJECT: 182,184,186 Gertrude St, North Gosford LOCATION: North Gosford SHEET: 1 OF 1 POSITION : E: 346164.590, N: 6301094.110 (56 MGA94) SURFACE ELEVATION: 32.800 (AHD) EQUIPMENT TYPE: Hand Auger METHOD: Hand Auger DATE EXCAVATED: 13/7/22 LOGGED BY: AT CHECKED BY: TH **EXCAVATION DIMENSIONS DRILLING** MATERIAL 100 200 HAND 300 & PENETRO-300 W METER CONSISTENCY RELATIVE DENSITY MOISTURE DCP TEST AS 1289.6.3.2-1997) Blows/150 mm PENETRATION SAMPLES & FIELD TEST DEPTH (m) SUPPORT GRAPHIC MATERIAL DESCRIPTION 500 STRUCTURE Soil Type, Colour, Plasticity or Particle Characteristic Secondary and Minor Components & Other Observations 0.0 SILTY CLAYEY SAND: dark brown, fine to medium grained sand, low to medium plasticity clay, with fine to medium grained gravel, with rootlets TOPSOIL STABLE FILL FILL: SILTY CLAYEY SAND: dark brown, fine to medium grained sand, fine to medium grained clay М 0.5 ğ RESIDUAL SOIL SILTY CLAY: brown, medium to high plasticity, with fine to medium grained sand VSt EXCAVATION HA4 TERMINATED AT 1.00 m 1.5 2.0 2.5 3.0 PHOTOGRAPHS NOTES YES NO NO CLASSIFICATION SYMBOLS & SOIL DESCRIPTION CONSISTENCY/ METHOD PENETRATION SAMPLES & FIELD TESTS RELATIVE DENSITY <u>шшт</u>= VS S F St Based on Unified - Very Soft - Soft U50 - Undisturbed Sample Natural Exposure No Resistance Classification System 50 mm diameter Existing Excavation - Firm - Stiff Disturbed Sample BH Backhoe Bucket MOISTURE VSt H VL - Very Stiff - Hard В **Bulk Disturbed Sample** Bulldozer Blade MC Moisture Content D - Dry M - Moist W - Wet Ripper WATER - Very Loose - Loose Hand Penetrometer (UCS kPa) 10 Oct., 73 Water Level on Date shown VS Vane Shear; P-Peak MD D VD SUPPORT - Medium Dense R-Remouded (uncorrected kPa) water inflow - Dense Timbering

PBT

water outflow

- Plate Bearing Test

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EXCAVATION NORTH GOSFORD.GPJ

RMS LIB 40.3

See Explanatory Notes for details of abbreviations & basis of descriptions.

- Very Dense

#### PIT NO: **EXCAVATION - GEOLOGICAL LOG** FILE / JOB NO: PROJECT: 182,184,186 Gertrude St, North Gosford LOCATION: North Gosford SHEET: 1 OF 1 POSITION : E: 346196.790, N: 6301106.610 (56 MGA94) SURFACE ELEVATION: 38.200 (AHD) EQUIPMENT TYPE: Hand Auger METHOD: Hand Auger DATE EXCAVATED: 13/7/22 LOGGED BY: AT CHECKED BY: TH **EXCAVATION DIMENSIONS DRILLING** MATERIAL 100 200 HAND 300 & PENETRO-300 W METER CONSISTENCY RELATIVE DENSITY MOISTURE DCP TEST AS 1289.6.3.2-1997) Blows/150 mm PENETRATION SAMPLES & FIELD TEST Ξ SUPPORT GRAPHIC MATERIAL DESCRIPTION 500 STRUCTURE DEPTH ( Soil Type, Colour, Plasticity or Particle Characteristic Secondary and Minor Components & Other Observations 0.0 SILTY CLAYEY SAND: dark brown, fine to medium grained sand, low to medium plasticity clay, with fine to medium grained gravel, with rootlets TOPSOIL STABLE FILL FILL: SILTY CLAYEY SAND: dark brown, fine to medium grained sand, fine to medium grained clay М 0.5 ğ SILTY CLAY: brown, medium to high plasticity, with fine to medium grained sand RESIDUAL SOIL VSt EXCAVATION HAS TERMINATED AT 1.00 m 1.5 2.0 2.5 3.0 PHOTOGRAPHS NOTES YES NO NO CLASSIFICATION SYMBOLS & SOIL DESCRIPTION CONSISTENCY/ METHOD PENETRATION SAMPLES & FIELD TESTS RELATIVE DENSITY <u>шшт</u>= VS S F St Based on Unified - Very Soft - Soft U50 - Undisturbed Sample Natural Exposure No Resistance Classification System 50 mm diameter Existing Excavation - Firm - Stiff Disturbed Sample BH Backhoe Bucket

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Bulldozer Blade

WATER

10 Oct., 73 Water Level on Date shown

water inflow

water outflow

Ripper

Timbering

See Explanatory Notes for details of abbreviations

& basis of descriptions.

SUPPORT

MOISTURE VSt H VL - Very Stiff - Hard В **Bulk Disturbed Sample** MC Moisture Content D - Dry M - Moist W - Wet - Very Loose - Loose Hand Penetrometer (UCS kPa) VS Vane Shear; P-Peak MD D VD - Medium Dense R-Remouded (uncorrected kPa) - Dense PBT - Plate Bearing Test - Very Dense

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#### PIT NO: **EXCAVATION - GEOLOGICAL LOG** FILE / JOB NO: PROJECT: 182,184,186 Gertrude St, North Gosford LOCATION: North Gosford SHEET: 1 OF 1 POSITION : E: 346170.690, N: 6301106.510 (56 MGA94) SURFACE ELEVATION: 34.700 (AHD) EQUIPMENT TYPE: Hand Auger METHOD: Hand Auger DATE EXCAVATED: 13/7/22 LOGGED BY: AT CHECKED BY: TH **EXCAVATION DIMENSIONS DRILLING** MATERIAL 100 200 HAND 300 & PENETRO-300 W METER CONSISTENCY RELATIVE DENSITY MOISTURE DCP TEST AS 1289.6.3.2-1997) Blows/150 mm PENETRATION SAMPLES & FIELD TEST Ξ SUPPORT GRAPHIC MATERIAL DESCRIPTION 500 DEPTH ( STRUCTURE Soil Type, Colour, Plasticity or Particle Characteristic Secondary and Minor Components & Other Observations 0.0 SILTY CLAYEY SAND: dark brown, fine to medium grained sand, low to medium plasticity clay, with fine to medium grained gravel, with rootlets TOPSOIL STABLE FILL FILL: SILTY CLAYEY SAND: dark brown, fine to medium grained sand, fine to medium grained clay М 0.5 ğ SILTY CLAY: brown, medium to high plasticity, with fine to medium grained sand RESIDUAL SOIL VSt EXCAVATION HA6 TERMINATED AT 1.00 m 1.5 2.0 2.5 3.0 PHOTOGRAPHS NOTES YES NO NO CLASSIFICATION SYMBOLS & SOIL DESCRIPTION CONSISTENCY/ METHOD PENETRATION SAMPLES & FIELD TESTS RELATIVE DENSITY VS S F St Based on Unified - Very Soft - Soft U50 - Undisturbed Sample Natural Exposure No Resistance Classification System 50 mm diameter Existing Excavation - Firm - Stiff Disturbed Sample BH Backhoe Bucket MOISTURE VSt H VL - Very Stiff - Hard В **Bulk Disturbed Sample** Bulldozer Blade MC Moisture Content D - Dry M - Moist W - Wet Ripper WATER - Very Loose - Loose Hand Penetrometer (UCS kPa) 10 Oct., 73 Water Level on Date shown VS Vane Shear; P-Peak MD D VD SUPPORT - Medium Dense R-Remouded (uncorrected kPa) water inflow - Dense Timbering

- Plate Bearing Test

PBT

water outflow

EXCAVATION NORTH GOSFORD.GPJ

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See Explanatory Notes for details of abbreviations

& basis of descriptions.

- Very Dense

## **About Cardno**

Cardno is a professional infrastructure and environmental services company, with expertise in the development and improvement of physical and social infrastructure for communities around the world. Cardno's team includes leading professionals who plan, design, manage and deliver sustainable projects and community programs. Cardno is an international company listed on the Australian Securities Exchange [ASX:CDD].

## Contact

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